

MODEL OF GENERALIZED MACHINE-TOOL

Sandu CONSTANTIN¹, Dana TILINĂ²

Rezumat. *Lucrarea de față prezintă un concept revoluționar și modern în care calculatorul poate modela o mașină-unealtă, determinând forma suprafețelor pieselor prelucrate pe aceasta cu o precizie mai mică de $0.01\mu\text{m}$. Acest concept a fost verificat în numeroase cazuri: prelucrarea roților dințate cilindrice cu freză melc, prelucrarea roților melcate cu determinarea liniilor de contact dintre melc și roata melcată, prelucrarea melcilor de la pompa de noroi; mașina de rectificat fără centre, unele aspecte ale prelucrării de finisare a roților dințate cilindrice prin șeveruire etc. Totodată, cu ajutorul lui se poate determina un model de prelucrare a pieselor în condiții de imprecizie reale ale mașinii și/sau de vibrații.*

Abstract. *This paper presents a revolutionary and modern concept according to whom the computer can mold and shape a machine tool, generating surfaces of the machined parts with an accuracy of less than $0.01\mu\text{m}$. This concept has been verified in many cases as: machining of cylindrical spur gears; machined worm wheel; parallel type worm manufacturing of solids handling pump; centerless grinding machine, some aspects of finishing cylindrical gears by shaving cutter, and so on. Also with the help of this concept can be determined the machining of the parts in conditions of real inaccuracy of the machine and / or vibration.*

Keywords: machine tool, surfaces, machining, model

1. Introduction

Surface treatment of the complex parts such as gears flanks led to the concept of generalized machine-tool. Machining with the gear hob is considered as among the most productive and economical methods [1, 2, 3]. Although technological process that is extended in production has still many aspects that can be improved to ensure increased gear performance in terms of accuracy and behavior in operation. In practice, calculation methods and adjustment of process parameters of technological system have limitations, especially in determining the size of processing errors and their classification in step precision prescribed.

This article presents theoretical aspects of generalized machine-tool [1, 4, 5]. According to the concept, it have been defined: the shape and position of the cutting edges and the cutting edges of the tool, the movements of the machine elements and assemblies, the timing of the movements, the part of the topographic surface and generating conditions.

¹Associate Professor PhD. Eng., Faculty of Engineering and Management of Technological Systems, University *Politehnica* of Bucharest, Romania (costel_sandu@yahoo.com).

²Lecturer PhD. Eng., Faculty of Engineering and Management of Technological Systems, University *Politehnica* of Bucharest, Romania (dana.tilina@upb.ro).

The cutting tool is one of the main elements of machining. It is processed on a machine tool that is also modeled. In conclusion cutting edges of the tool are determined by the generalized machine-tool.

2. Theoretical aspects

The literature presents theoretical and numerical rating on generating complex surfaces [6, 7], referring to the teeth flanks cylindrical spur wheels, inclined or curved. These are based on the establishment and application of computer programs that determines the shape of various surfaces for reasons of machine parts without defining them by working on machine tools.

There are presented important aspects of processing desired parts that would be difficult to put out without any extensive time and money.

Theoretical generation of surfaces received a boost particularly by defining their two theoretical curves: generating curve (G) and guiding curve (D).

The application of the generalized machine-tool highlights the influence of geometrical parameters of the tool and of the gear, their position, cinematic errors, the influence of vibrations on the machined surface, machine control errors and elastic deformations [1, 8].

Accuracy of machined surfaces [9, 10] is influenced by the type adjustment items that are considered as input data.

2.1. Part definition

Part definition is performed by shaping the outer surface of the blank and "topographic" surfaces. The topographic surfaces are flat surfaces, cylindrical, spherical, etc., as defined within the blank.

2.2. Basic elements

Being given a part where there is a cylindrical shape blank and which are defined topographic surfaces such as perpendicular planes to the cylinder axis (Fig. 1). Other forms of topographic surfaces are cylinders, cones, spheres and so on. It is considered a cutting edge (T0), defined by a number of points (A, B, C, D, E), where the relative movement of the tool from the piece, intersect topographic surfaces successively in points (A1, B2, C3, D4, E5). The point E of the cutting edge describe de curve (C) (E0, E1, E2, E3, E4, E5) called the guiding curve.

The curve (A1, B2, C3, D4, E5) can not be assimilated in most cases with the guiding curve. The curve represents the intersection of the cutting edge with the topographic surface and will be called „trace” and is a component of the cutting scheme.

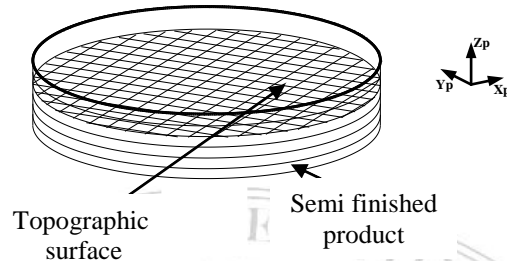


Fig. 1. Topographic surface of the cylindrical blank.

2.3. The tool

If the cutting tool is in the initial position (T0), during the relative movement performed during time (w) will occupy the positions (T1), (T2), (T3), (T4) and (T5) at the time w_1, w_2, w_3, w_4 and w_5 (Figure 2).

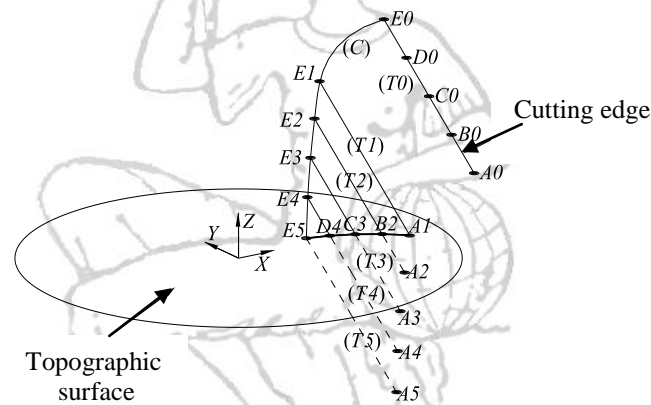


Fig. 2. Traces of machining the topographic surface.

To define the cutting edges we give as an example the lathe tool (Figure 3).

The cutting edge is in this case the curve ABCD where AB is the main cutting edge; BC is the cutter bit and CD is secondary cutting edge.

In this case the cutting edge of figure 2 (T0) becomes the ABCD curve that defines a lot of waypoints which define the final curve that determines the tracks in the topographic surface.

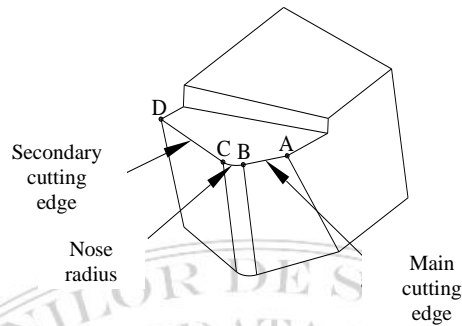


Fig. 3. Cutting edge of the lathe tool.

Cutting tools like cutters, drills, broaches, and so on, have a similar number of cutting edges similar to the ABCD curve in figure 3, which is called tooth (Fig. 4.).

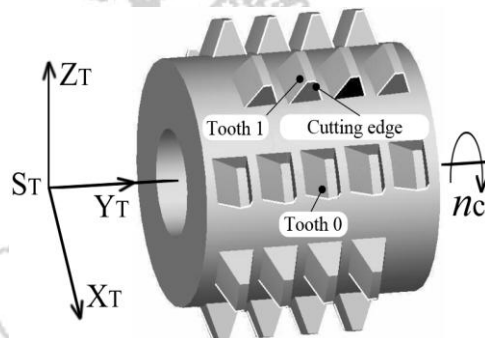


Fig. 4. Teeth and cutting edges of the spline hob.

Conceptually, for the spline hob above, the file for 33 teeth contains the following:

```

720 30.625 -17.68277 .2168031 39.375 -20.86354 5.776781E-02
720 39.375 -23.1737 -5.774027E-02 30.625 -26.35447 -.2167817
675 21.80845 -16.30661 -21.50184 27.88318 -19.48738 -27.80148
675 27.8015 -21.79754 -27.88316 21.50186 -24.97831 -21.80843
....
0 30.625 4.335847 .2167924 39.375 1.155081 5.775404E-02
0 39.375 -1.155081 -5.775404E-02 30.625 -4.335847 -.2167924
....
-675 21.50186 24.97831 21.80843 27.8015 21.79754 27.88316
-675 27.88318 19.48738 27.80148 21.80845 16.30661 21.50184
-720 30.625 26.35447 .2167817 39.375 23.1737 5.774027E-02
-720 39.375 20.86354 -5.776781E-02 30.625 17.68277 -.2168031

```

2.4. Machine structure, coordinate systems, axes and generating movements

The real machine-tool for milling spur gears, which is used for generalized machine-tool modeling, has a number of subassemblies, where: 1-frame; 2-pillar; 3- vertical slide; 4- hub slide; 5- weight slide port; 6-generation plane with $z = 0$; X_f, Y_f, Z_f - fixed coordinate system (Figure 5).

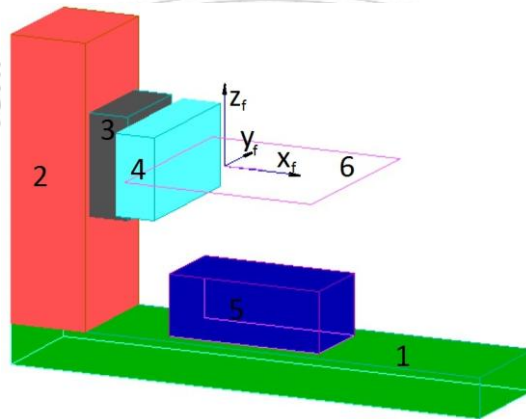


Fig. 5. Cylindrical gear milling machine structure with fixed coordinate systems.

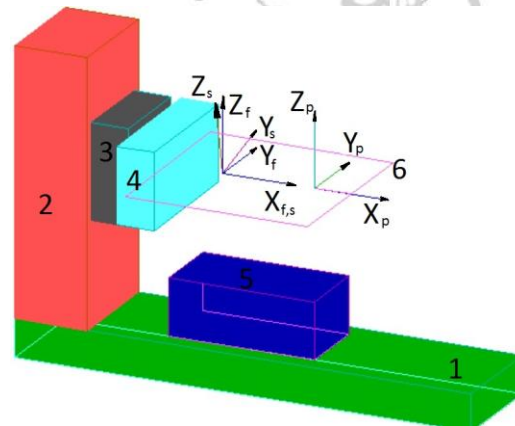


Fig. 6. Cylindrical gear milling machine structure with coordinate systems.

2.5. Reference systems and movements

For working with generalized machine-tool, three coordinate systems are used: the machine (O_f, X_f, Y_f and Z_f); the tool (O_s, X_s, Y_s and Z_s), and the part (O_p, X_p, Y_p and Z_p) (Figure 6). The coordinate system of the machine is fixed against the machine, and the others are programmed with shift their origin (O_s or O_p) from O_f and / or translational parameterized while the origins O_s or O_p along axes: X_f, Y_f , or Z_f . The coordinate system is programmed with parameterized rotation around his own axis.

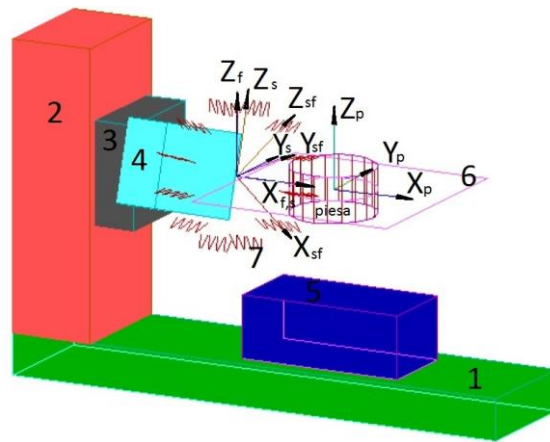


Fig. 7. Cylindrical gear milling machine structure with processing coordinate: 1-frame; 2-pillar; 3-vertical slide; 4- hub slide; 5- weight slide port; 6-generation plane with $z = 0$; 7-cutting edges; X_f, Y_f, Z_f - fixed coordinate system; X_s, Y_s, Z_s - coordinate system of the tool X_p, Y_p, Z_p - coordinate system of the part; X_{sf}, Y_{sf}, Z_{sf} - coordinate system of the cutting tool.

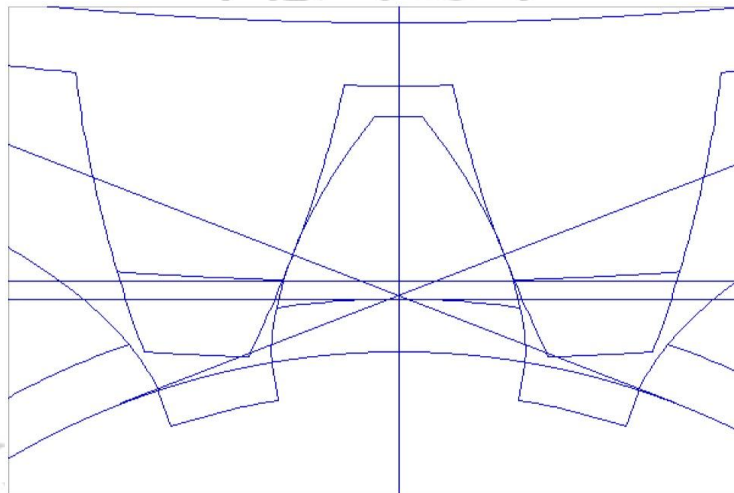


Fig. 8. The representation of the gear after data input.

2.6. Data input

For the determination tool path is necessary to introduce the following data:

- cutting edges and raw material (Figure 7).
- part parameters (Figure 8).

After entering this data we can pass to the next stage, the generalizes machine-tool functioning.

3. Surface generation mathematics

The starting point is the cutting edge [1]. Their mathematical expression, in parametric form, is:

$$C_e : \begin{cases} x_t = x_t(u) \\ y_t = y_t(u) \\ z_t = z_t(u) \end{cases}, \quad (1)$$

In which the u parameter defines the points.

3.1. Transformation matrix

The characteristics and movements directions are defined (Figure 7).

For analytical expression of achieved trajectories, we are using a matrix of the following form:

$$[M]: \begin{bmatrix} x_1 & y_1 & z_1 & M_1 & F_1(w) \\ x_2 & y_2 & z_2 & M_2 & F_2(w) \\ x_3 & y_3 & z_3 & M_3 & F_3(w) \\ \dots & & & & \\ x_n & y_n & z_n & M_n & F_n(w) \end{bmatrix} \quad (2)$$

It is considered $x_1, x_2, \dots, x_n, y_1, y_2, \dots, y_n$ and z_1, z_2, \dots, z_n values of the displacements of the translational axes X, Y respectively Z of the current coordinate system, to the previous coordinate system. For example, x_2, y_2, z_2 are displacements of the coordinate system S_2 to system S_1 .

Notations M_1, M_2, \dots, M_n expresses the type of transformation between considered reference systems (example: if M_2 is t_x , it represents translational movement in X system S_2 to S_1 , if M_2 is r_z , performing a rotation movement around the Z axis system S_2 to S_1). Elements of the fifth column of the matrix $[M]$, denoted $F_1(w), F_2(w), \dots, F_n(w)$ define parametric (w) movements along the indicated axis by element on the line of the column to fourth matrix.

4. Generalized machine-tool

The generalized machine-tool functioning is based on a comprehensive calculation program developed and checked for various practical applications. There were designed algorithms for calculating the surface generation in accordance with those described in [1], to which is added algorithms for entering data that define the part (execution document), regulatory mechanisms and characteristics of the machine kinematic chains. The output algorithms are variables or graphics on the gear and its tooth flanks.

The computation programme has a modular structure with communication interfaces with the operator and machine. The communication interfaces successively open for data input and output, for representations and results of operation of the machine in question.

5. Numerical results

Applying the concept of generalized machine-tool enables rapid determination, graphically and numerically different basic aspects of the teeth gap generation. The generalized machine-tool is designed with high modular flexibility. If the defining movements contains harmonic functions we can determine the shape of the generated flanks under vibration conditions.

5.1 Removing the stock left for machining

By moving cutting tool, the traces of each tooth of the tool in the topographic surface represent the section of the cutting chips removed from the part. All of these traces represent the cutting scheme (Figure 9).

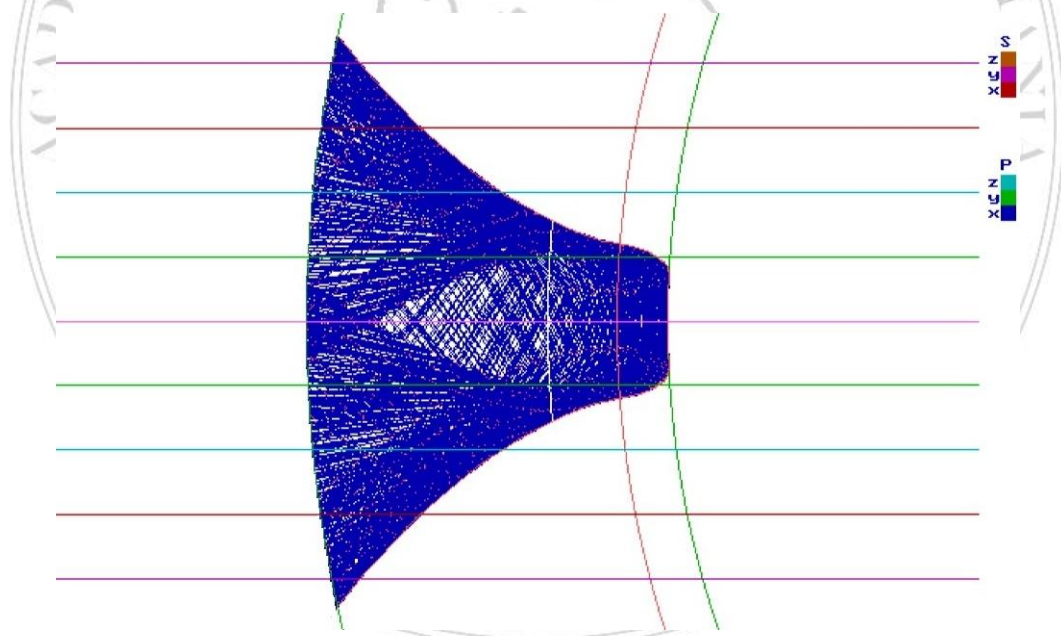


Fig 9. The milling sketch.

5.2. Tooth profile

It is the last stage of the generalized machine-tool use in which is presented the sprocket profile in connection with the gear and can be easily track the gearing movement (Figure 10).

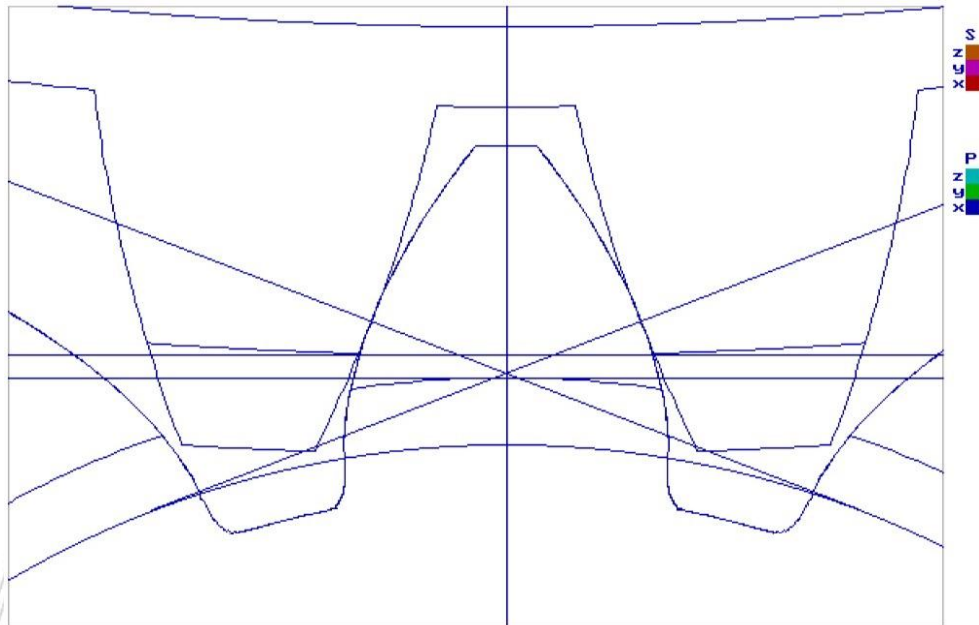


Fig.10. Representation of the gear after data input and of the sprocket determined by generalized machine-tool.

Conclusions

The generalized machine-tool is an extremely useful instrument for:

- the machine-tool design engineer, for machining complex surfaces and in determining the kinematics of the machine;
- the user by knowing the surfaces of the part under certain adjustment conditions of the machine, the cutting tool used with or without vibrations during the machining.

Depending on the measurement of the deviations in moving the machine elements, we can determine the correction values for the CNC machines in order to obtain the values from the nominal data.

By using different modeling and by comparing the results obtained with the generalized machine-tool to those obtained in real manufacturing, the results were validated.

REFERENCES

- [1] C. Sandu, *Contributions regarding the improvement of the dynamic qualities of the rolling linkage of the gear processing machine*, PhD Thesis, Polytechnic Institute, Bucharest, **1987**.
- [2] K.D. Bouzakis., E. Lili, N. Michailidis, O. Friderikos, *Manufacturing of cylindrical gears by generating cutting processes: A critical synthesis of analysis methods*. CIRP Annals-Manufacturing Technology , pp. 676-696, **2008**.
- [3] H. Pfauter, *Wälzfräsen, Teil 1: Verfahren, Maschinen, Werkzeuge, Anwendungstechnik, Wechselräder*, Springer-Verlag, Berlin, Heidelberg, New York, ISBN 3-540-07446-5, (1976)
- [4] C. Sandu, Co. Sandu, G. Dobre, *New Principles for Surface Generation Starting from the System Machine Tools and Tools*, Scientific Bulletin of North University of Baia Mare, Series C, Volume XIV, pp. 233-238, România, **2000**.
- [5] G. Sandu, *Generarea suprafețelor*, Editura Academiei Române, București, ISBN 978-973-27-1730-1, **2000**.
- [6] F. L. Litvin, A. Fuentes, *Gear geometry and applied theory*, Cambridge University Press, ISBN 0-521-81517-7, USA, (**2004**).
- [7] G. Henriot, *Engrenages, Conception, fabrication, mise en œuvre*. 8^e édition, Dunod Publishing, ISBN 978-2100599936, (**2013**).
- [8] K.D. Bouzakis, O. Friderikos, I. Tsiafis, *FEM-supported simulation of chip formation and flow in gear hobbing of spur and helical gears*. CIRP Journal of Manufacturing Science and Technology **nr. 1**, ISSN: 1755-5817, pp. 18-26, **2008**.
- [9] A. Ghionea, *Contributions to the study of generation process of polyhypocycloidal teeth*. PhD Thesis, "Politehnica" Institute of Bucharest, **1987**.
- [10] A. Ghionea, I. Mașala, *Contributions of the kinematic generation study of the involute profile*. Technologies, Quality, Machines, Materials, International Conference on Manufacturing Systems ICMaS'98, Technical Publishing, pp. 245-250, Bucharest, ISBN 973-31-1238-0, **1998**.
-